



DIVISIÓN DE EDUCACIÓN
CONTINUA Y A DISTANCIA



Del 08 al 10 de Noviembre de 2007

EXPOSITOR: ING. FERNANDO TOLEDO TOLEDO

SECRETARÍA DE LA DEFENSA NACIONAL



PARÁMETROS DE LÍNEAS DE TRANSMISIÓN

Tanto la inductancia como la capacitancia de una Línea de Transmisión (LT) dependen de la configuración geométrica, el arreglo que tienen los conductores en la estructura de soporte, poste, torre o ducto.

Este aspecto es significativamente importante sobre todo para las LT aéreas, debido a que representan un alto porcentaje del total de las líneas en redes de potencia. Aquí, el dieléctrico es el aire y el límite térmico de conducción de corriente (ampacidad) es mucho más alto que en el caso de las líneas de transmisión subterráneas, en donde el aislante utilizado representa una limitación térmica importante. Los parámetros RLC en una LT se encuentran distribuidos uniformemente (figura 1).

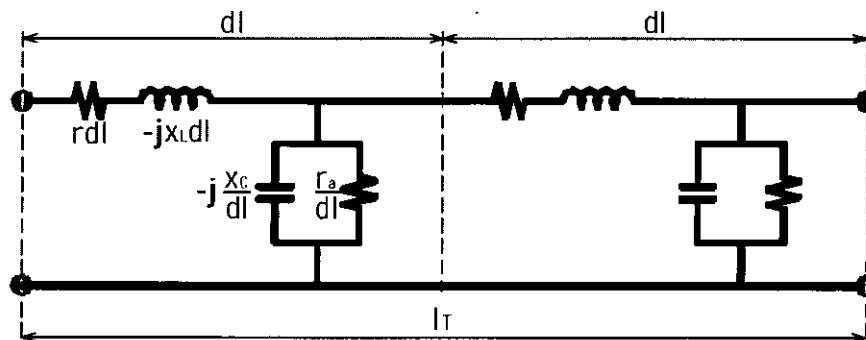


Figura 1. Parámetros de una línea de transmisión.

Donde:

- r : Resistencia por unidad de longitud Ω/km .
- x_L : Reactancia inductiva por unidad de longitud Ω/km .
- x_C : Reactancia capacitiva por unidad de longitud $\Omega \cdot \text{km}$.
- r_a : Resistencia de aislamiento por unidad de longitud $\Omega \cdot \text{km}$.

Una vez conocidos los parámetros por unidad de longitud de la LT, podemos calcular la resistencia total por fase de la línea:

$$R \approx r l_T$$

donde:

l_T : longitud total de la línea.

$$X_L \approx x_L l_T$$

$$X_C \approx \frac{x_a}{l_T}$$

$$R_a \approx \frac{r_a}{l_T} = \text{resistencia de aislamiento total por fase.}$$

$$Z_S \approx r + jx_L = \text{impedancia serie por unidad de longitud.}$$

$$Z_P \approx \frac{-jx_C r_a}{r_a - jx_C} = \text{impedancia paralelo por unidad de longitud.}$$

Se pueden tomar dos tipos de modelos para LT.

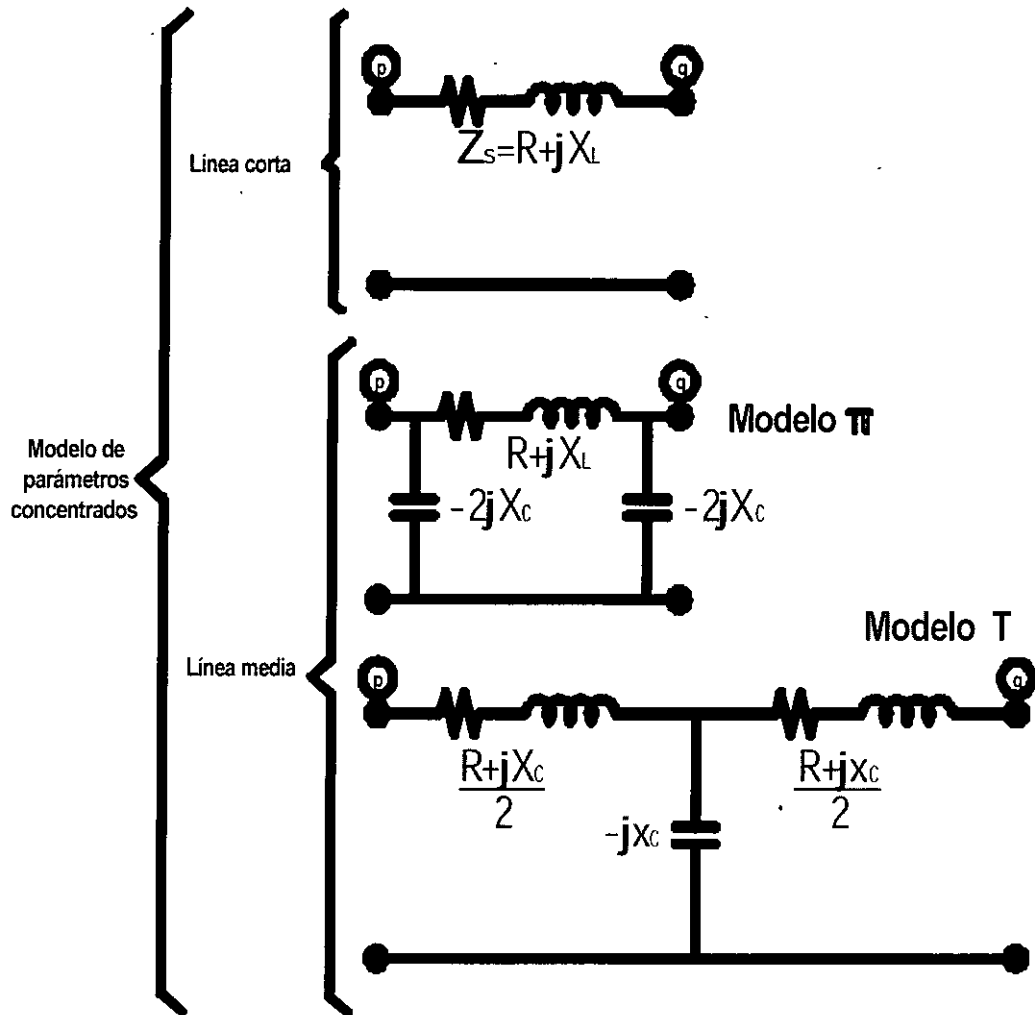


Figura 2. Modelo de parámetros concentrados.

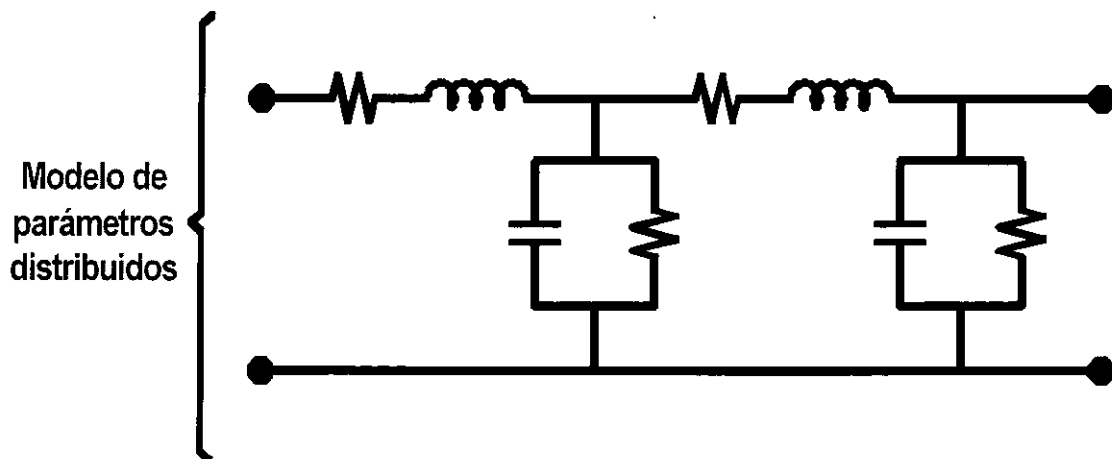


Figura 3. Modelo de parámetros distribuidos.

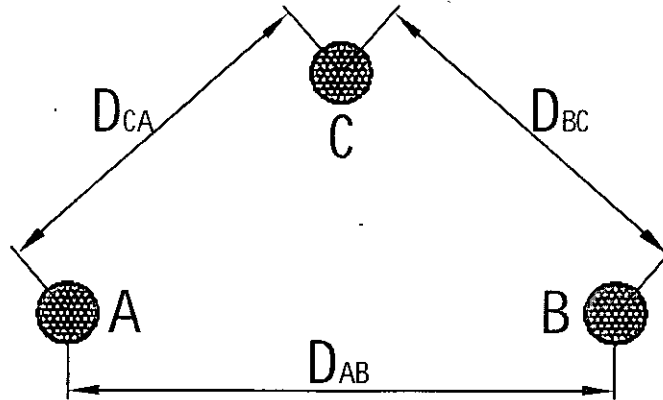


Figura 4. Línea de transmisión con un conductor por fase.

Inductancia (para circuitos trifásicos): Este parámetro está en función de líneas de flujo magnético producidas por otro conductor y enlazado por el conductor. El número de líneas de flujo enlazados depende de la intensidad de campo magnético y de la distancia.

La inductancia por fase por unidad de longitud, es:

$$L \approx 2 \times 10^{-7} \ln \frac{DMG}{RMG} \text{ H/m}$$

donde:

DMG: Distancia media geométrica de las distancias de separación entre conductores: $DMG = \sqrt[3]{D_{AB} D_{BC} D_{CA}}$

D_{AB} , D_{BC} , D_{CA} : Flujo magnético enlazado por los conductores.

RMG: Radio Medio Geométrico.

Para que el flujo magnético enlazado sea el mismo es necesario transponer las líneas (figura 5), así las impedancias por fase se equilibran.

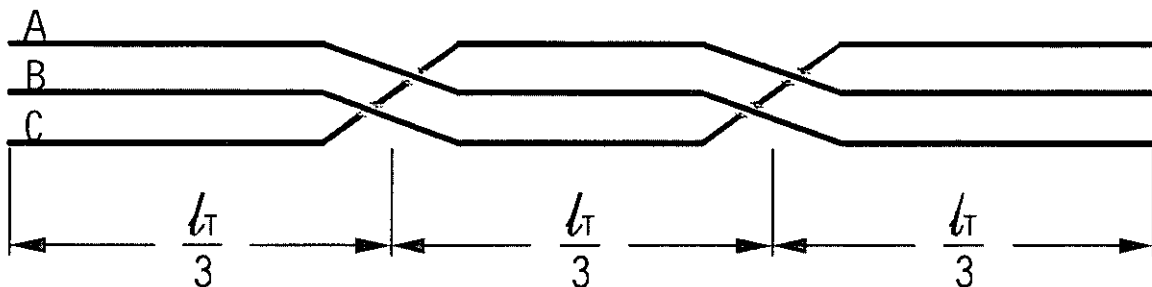


Figura 5. Flujo magnético igual en toda la LT.

El flujo total producido por el conductor puede agruparse en:

Flujo interno: que es producido por el conductor pero interno a él.

Flujo externo: producido por el conductor externo a él.

Se define el radio medio geométrico como el radio de un conductor hipotético de pared infinitesimal (hueco) de tal manera que el flujo total es exterior a él y equivalente al del conductor original.

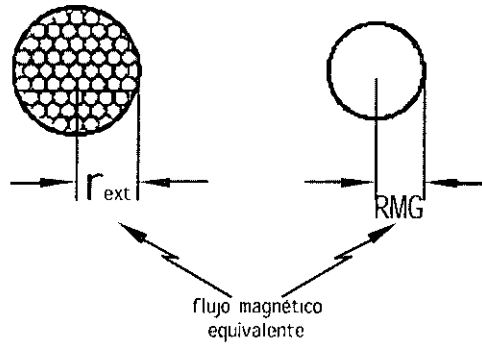


Figura 6. Radio Medio Geométrico.

Los conductores pueden ser cables o alambres (figura 6), de cobre (Cu) o de aluminio (Al) del tipo ASCR (conductor de aluminio con alma de acero), de tal manera que para conductores sólidos $RMG = r_{ext} e^{-1/4}$.

Ejemplo 1:

Sea una LT con 2CF, tal como se muestra en la figura 7 (transpuesta).

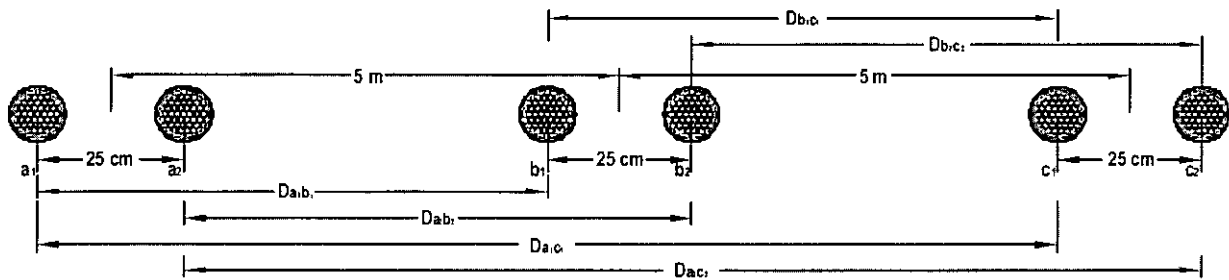


Figura 7. Configuración de la línea de transmisión del ejemplo.

Obtener la DMG del arreglo

$$D_{a_1 b_1} = D_{a_2 b_2} = D_{b_1 c_1} = D_{b_2 c_2} = D_1 = 500 \text{ cm}$$

$$D_{b_1 c_2} = D_2 = 525 \text{ cm}$$

$$D_{b_2 c_1} = D_3 = 475 \text{ cm}$$

$$D_{a_1 c_1} = D_{a_2 c_2} = D_4 = 1000 \text{ cm}$$

entonces

$$DMG = \sqrt[4]{D_1^4 \cdot D_2^2 \cdot D_3^2 \cdot D_4^2 \cdot D_{a_1 c_2} \cdot D_{a_2 c_1}} = \sqrt[4]{D_1^4 \cdot D_2 \cdot D_3 \cdot D_4 \cdot D_{a_1 c_2} \cdot D_{a_2 c_1}}$$

$$DMG = \sqrt[4]{500^4 \cdot 525 \cdot 475 \cdot 1000 \cdot 1025 \cdot 975} = \sqrt[4]{3.88431395 \times 10^{33}}$$

$$DMG = 629.6649614 \text{ cm}$$

RADIO MEDIO GEOMÉTRICO PARA ARREGLOS MULTICONDUCTORES.

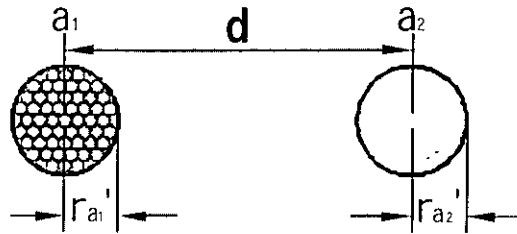


Figura 8. Radio Medio Geométrico para un arreglo de dos conductores por fase.

El RMG es un valor que representa un radio hipotético, este radio es siempre menor que el radio exterior designado con r' el RMG, para la figura 1.

$$RMG_A \approx \sqrt[4]{r_{a1}' d_{a1a2} r_{a2}' d_{a2a1}}$$

Si se tienen conductores iguales (como es común), entonces:

$$RMG_A \approx \sqrt{r_a' d_{a1a2}}$$

$$RMG_{ABC} \approx \sqrt[3]{RMG_A RMG_B RMG_C}$$

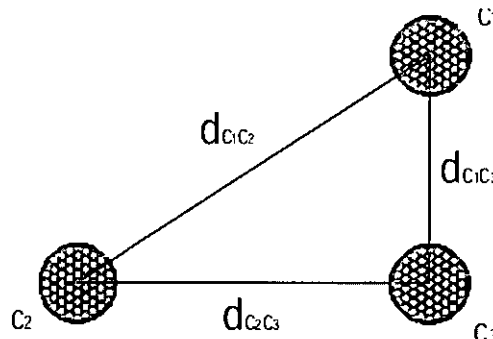


Figura 9.

$$RMG_C \approx \sqrt[6]{r_{a1}' r_{a2}' r_{a3}' d_{C1C2} d_{C1C3} d_{C2C3}}$$

$$Z_s \approx R + jX_L \approx \frac{1}{f}$$

$$X_L \approx 2\pi f L_T$$

L_T : Inductancia total de la línea $L_T \approx L l_T$

L : Inductancia por unidad de longitud.

l_T : Longitud total.

Z_s : Es una limitancia fundamental de la capacitancia de transferencia de la LT (es indispensable que Z_s sea pequeña).

$$L \approx 2 \times 10^{-7} \ln \frac{DMG}{RMG} \frac{f}{m}$$

Existen dos denominaciones para el calibre de conductores:

- 1) **CU** Circular Mils: Medida de área de un círculo que tiene como radio una milésima de pulgada.
- 2) **AWG** American Wire Gage: Galgas Americanas de conductor.

Los materiales empleados en conductores para LT, son:

- Cobre (Cu).
- Aluminio (Al).
- Acero (operativamente como refuerzo).

Ejemplo 2:

Sea una LT (transpuesta), con $l_T = 40\text{km}$ y 3.5m de separación entre conductores de cobre de 250MCM con 12 hilos (fig. 10) a 6.9kV .

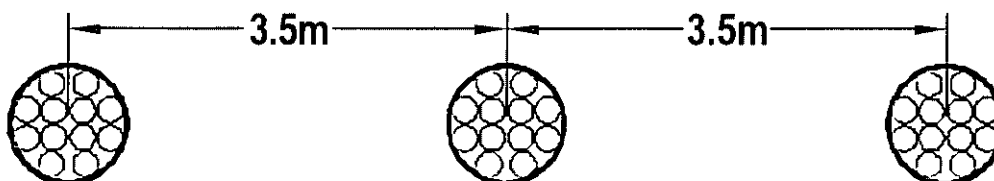


Figura 10. Línea de Transmisión del ejemplo.

Determine:

- a) Impedancia serie por unidad de longitud.

$$Z_s = r + jX_L \text{ (O/km)}.$$

- b) Impedancia total por fase (O/fase).
- c) Cálculo con tablas.

Solución:

Sea $r = r_a 0.257 \text{ O/milla} = 0.159726538 \text{ O/km}$

$$X_L = 2\pi f \cdot 2 \times 10^{-7} \ln \frac{DMG}{RMG}$$

entonces:

$$DMG = \sqrt[3]{3.5 \cdot 3.5 \cdot 3.5} = 4.409723675 \text{ m}$$

$$RMG = 0.01902 \text{ ft} = 5.797296 \times 10^{-3} \text{ m}$$

$$X_L = 2\pi (60\text{Hz}) \cdot 2 \times 10^{-7} \ln \frac{4.409723675 \text{ m}}{5.797296 \times 10^{-3} \text{ m}}$$

$$X_L = 0.5002050638 \times 10^{-3} \text{ / m} = 0.5002050638 \text{ / km}$$

$$Z_s = (0.159726538 + j 0.5602050638) \text{ O/km}$$

Que es la impedancia serie por unidad de longitud.

CAPACITANCIA Y REACTANCIA CAPACITIVA.

La capacitancia está en relación con el campo eléctrico este emana radialmente del exterior de los conductores que tienen potencial. El valor de la capacitancia depende de la distancia de separación y de las características del medio dieléctrico.

$$C_n = \frac{0.02412 k}{\log_{10} \frac{DMG}{RMG_c \sqrt{4HMG^2 - DMG^2}}} \text{ } \frac{F}{\text{km fase}}$$

$$X_n = \frac{6.596}{f k} \log_{10} \frac{DMG}{RMG_c \sqrt{4HMG^2 - DMG^2}} \text{ } \frac{M}{\text{km}}$$

Valores por unidad de longitud

Es un parámetro que por su valor en algunos casos se desprecia para una LT aérea depende fundamentalmente de su voltaje nominal y de su longitud. Estos parámetros establecen (como se verá más adelante), la clasificación de la LT.

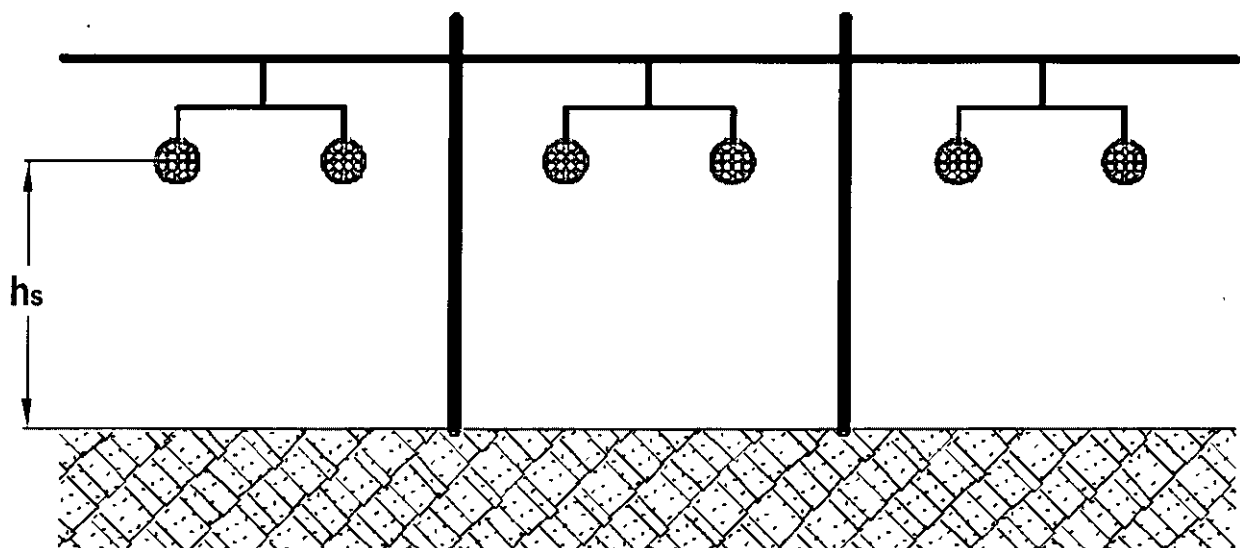
De las expresiones de Cn y Xc descritas arriba, los parámetros asociados son:

K: Constante dieléctrica del medio aislante. Para el aire k=1.

DMG: Distancia media geométrica (igual a la utilización en el cálculo de la inductancia).

RMGc: Radio medio geométrico considerando radios individuales externos (no radios utilizados en el cálculo de inductancias).

HMG: Altura media geométrica¹, considerando las alturas de los conductores sobre la estructura de soporte (figura 11) y el perfil de los mismos en el claro intercostal (figura 12).



¹ Considerando el efecto de la tierra (suelo) sobre la capacitancia.

Figura 11.

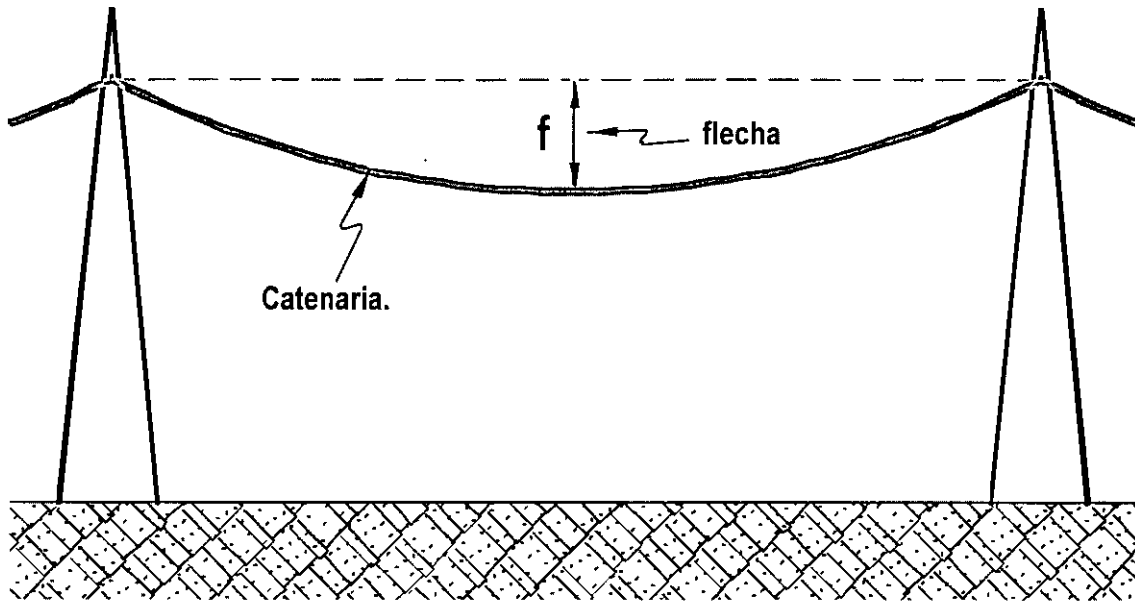


Figura 12.

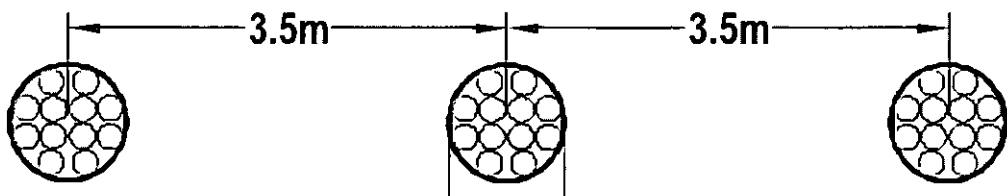
Altura media: $h_b = -0.7f$ con una frecuencia de 60Hz. Si se trata de una línea de transmisión o subtransmisión hasta 115kV (MT) ? $HMG \gg DMG$ y entonces:

$$\frac{2HMG}{\sqrt{4HMG^2 + DMG^2}} \approx 1, \text{ con } k=1 \text{ para todas las líneas aéreas.}$$

$$\text{De donde: } C_n \approx \frac{0.02412 \cdot F}{\log_{10} \left(\frac{DMG}{RMG_e} \right)} \text{ /km fase}$$

Ejemplo 3:

Para el ejemplo 2 de estudio (1CF) determine la capacitancia y reactancia capacitiva por unidad de longitud y total de la línea (ver ejemplo 2 y figura 13).



13.

Figura

Solución:

Como se mencionó arriba, con la expresión para C_n , en el caso donde se tiene 1CF, RMG_c es el radio exterior, el diámetro exterior en éste caso es $r_{ext}=0.6$ pulg.=0.01524m y $DMG = 14.4676ft = 4.4097m$, de tal modo que:

$$RMG_c = \frac{r_{ext}}{2} = \frac{0.01524}{2} = 7.62 \times 10^{-3} m$$

Luego, la capacitancia al neutro por unidad de longitud es calculada de la siguiente manera:

$$C_n = \frac{0.02412 k}{\log_{10} \frac{DMG}{RMG_c}} = \frac{0.02412}{\log_{10} \frac{4.4097m}{7.62 \times 10^{-3} m}} = 8.731367 \times 10^{-3} F/km$$

La capacitancia total por fase:

$$C_T = C_n \cdot l_T = 8.731367 \times 10^{-3} F/km \cdot 40km$$

$$C_T = 0.349255 F/fase$$

Análogamente la reactancia capacitiva por unidad de longitud es:

$$x_c = \frac{1}{2\pi f C_n} = \frac{1}{2\pi \cdot 60Hz \cdot 8.731367 \times 10^{-3} F/km}$$

$$x_c = 0.303799 M/km$$

La reactancia capacitiva total:

$$X_c = \frac{x_c}{l_T} = \frac{0.303799 M \cdot km}{40km} = 7.59498 \times 10^{-3} M/fase$$

Finalmente determinamos x_c y X_c por tablas. Así, de la tabla 8 tenemos:

$$14 ft = 0.0781 \text{ milla}$$

$$15 ft = 0.0803 \text{ milla}$$

de tal manera que para 1ft calculamos por regla de tres $0.0022 \text{ milla} = 1.028714192 \times 10^{-3} ft$

$$x_c = 0.0781 \cdot 1.028714192 \times 10^{-3}$$

$$x_c = 8.03425784 \times 10^{-6} \text{ milla}$$

LÍNEA DE TRANSMISIÓN TRANSPUESTA.

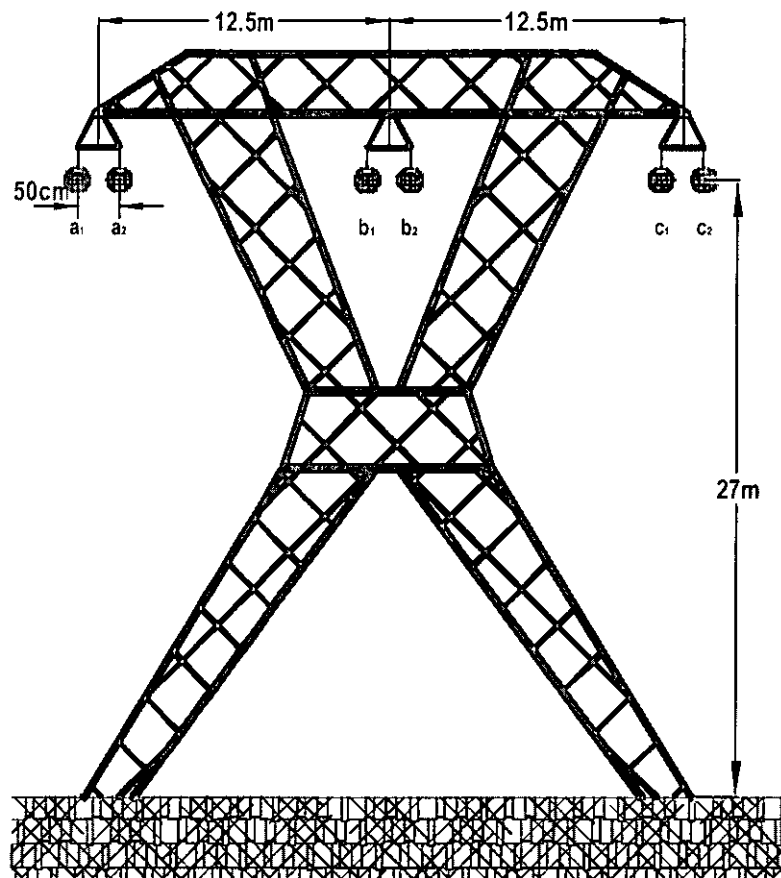


Figura 14.

Ejemplo 4.

Conductor ACSR $r_{ext}=32\text{mm}$, calibre 1033.5MCM, $l_T=350\text{km}$, $f=15\text{m}$ y $V_{nom}=400\text{kV}$.

1. Determinar de acuerdo a tablas cual es el conductor más cercano y tomarlo como dato.
2. calcular las impedancias serie y paralelo por unidad de longitud y total de la línea.

Solución:

$$r_{ext} = 32\text{mm} \cdot \frac{1\text{pulg}}{25.4\text{mm}} = 1.2598\text{pulg}$$

$$r_{ext} = 1.246\text{pulg}$$

Por otra parte, de tablas tenemos $RMG = 0.0420\text{ft}$ y de un conductor por fase $x_a = 0.3850\text{ conductor/milla}$.

$$RMG = 0.0420 \text{ ft} \left\{ \frac{0.3048 \text{ m}}{1 \text{ ft}} \right\} = 0.0128016 \text{ m}$$

$$RMG = 0.0128016 \text{ m} = r_{a_1} = r_{b_1} = r_{c_1}$$

$$RMG_A = RMG_B = RMG_C$$

$$RMG_A = \sqrt{r_{a_1} d_{a_1 a_2}} = \sqrt{0.0128016 \text{ m} \cdot 0.5 \text{ m}}$$

$$RMG_A = 0.080005 \text{ m} = 0.2625 \text{ ft}$$

Luego el radio medio geométrico del arreglo es:

$$RMG_{ABC} = \sqrt[3]{RMG_A RMG_B RMG_C} = RMG_A$$

$$RMG_{ABC} = 0.2625 \text{ ft} = 0.080005 \text{ m}$$

$$DMG_{ABC} = \sqrt[3]{DMG_{AB} DMG_{AC} DMG_{BC}}$$

$$DMG_{AB} = \sqrt[4]{d_{a_1 b_1} d_{a_1 b_2} d_{a_2 b_1} d_{a_2 b_2}} = DMG_{BC}$$

donde

$$d_{a_1 b_1} = d_{a_2 b_2} = 12.5 \text{ m}$$

$$d_{a_1 b_2} = 13 \text{ m}$$

$$d_{a_2 b_1} = 12 \text{ m}$$

$$DMG_{AB} = \sqrt[4]{12.5^2 \cdot 13 \cdot 12} = 12.495 \text{ m} = DMG_{BC}$$

$$DMG_{AC} = \sqrt[4]{25^2 \cdot 25.5 \cdot 24.5} = 24.998 \text{ m}$$

$$DMG_{ABC} = \sqrt[3]{12.495^2 \cdot 24.998} = 15.744 \text{ m}$$

Entonces la inductancia por unidad de longitud:

$$L = 2 \times 10^{-7} \ln \left(\frac{DMG}{RMG} \right) \left(\frac{\text{H}}{\text{m}} \right) = 2 \times 10^{-7} \ln \left(\frac{15.744 \text{ m}}{0.080005 \text{ m}} \right) \left(\frac{\text{H}}{\text{m}} \right)$$

$$L = 1.05643 \text{ } \mu\text{H/m}$$

La reactancia inductiva por unidad de longitud.

$$x_L = 2 \pi f L = 2 \pi \cdot 60 \text{ Hz} \cdot 1.05643 \text{ } \mu\text{H/m}$$

$$x_L = 0.3983 \text{ } \Omega/\text{km}$$

Análogamente la impedancia serie por unidad de longitud es $Z_s = r + j x_L$, en donde r es la resistencia por unidad de longitud que de acuerdo a tablas

$$r = 0.0565 \text{ } \Omega/\text{conductor}/\text{km}.$$

Pero tenemos dos conductores, entonces $r = \frac{0.0565 \text{ } \Omega \cdot \text{conductor/km}}{2 \text{ conductores}} = 0.0282 \text{ } \Omega / \text{km}$.

Así, la impedancia es finalmente:

$$z_s = 0.0282 + j 0.3982 \text{ } \Omega / \text{km} \cdot \text{fase}$$

Del mismo modo, la impedancia serie total por fase de la línea, es:

$$Z_s = z_s l_T = (0.0282 + j 0.3982 \text{ } \Omega / \text{km}) (350 \text{ km})$$

$$Z_s = 9.87 + j 139.37 \text{ } \Omega / \text{fase} = 139.72 \angle 85.95^\circ \text{ } \Omega / \text{fase}$$

donde la relación x/r está determinada por:

$$\frac{x}{r} = \frac{139.37}{9.87} = \tan 85.95^\circ = 14.12$$

SECCIÓN DE CONDUCTORES

En la práctica, las secciones de conductores se mide en mm², cm², in², CM (circular mil). El CM es la unidad del sistema ingles cuya definición es la siguiente: Un CM es el área de un círculo cuyo diámetro es una milésima de pulgada.

$$CM = \frac{D^2}{4} \cdot 10^{23} \text{ ? } \frac{D^2}{4} \cdot 10^{16} \text{ pulg} \dots\dots\dots(1)$$

Si calculamos el área de una sección circular con el diámetro expresado en pulgadas se tiene:

$$A = \frac{D^2}{4} \text{ pulg}^2 \dots\dots\dots(2)$$

Para expresar ésta área (2) en CM realizamos

$$\frac{A}{CM} = \frac{\frac{D^2}{4}}{\frac{D^2}{4} \cdot 10^{16}} \text{ ? } A = 10^{16} D^2 (CM) \quad \text{donde D es el diámetro} \dots\dots\dots(3)$$

En nuestro país se ha adoptado la norma AWG (American Wire Gage) con las siguientes especificaciones.

- a) El conductor más grueso es el número 4/0 que tiene un diámetro de 0.460in y el más delgado del número 36 que tiene un diámetro de 0.005 pulg.
- b) Entre el conductor 4/0 y el número 36, se tienen 38 calibres intermedios que se designan con diámetro decreciente, de la siguiente manera: 4/0, 3/0, 2/0, 1/0, 1, 2, 3, 4, ..., 36; es decir la norma consta de 40 calibres.
- c) Los diámetros forman la progresión: D, Dr, Dr², Dr³, ..., Dr³⁹. Donde D=0.460pulg y

$$Dr^{39} = 0.005 \text{ pulg} \quad \text{ ? } r = \sqrt[39]{\frac{0.005}{0.460}} = 0.8905257 \dots\dots\dots(4)$$

con $D_n = Dr^{(n-1)} = D_n \cdot r = \frac{D_n \cdot r^n}{r^{(n-1)}}$? $r = 0.8905257$

$$\text{ ? } D_{n+1} = 0.8905257 \cdot D_n \dots\dots\dots(5)$$

De tal manera que de la ecuación (5) observamos que a medida que el número de calibre aumenta, el diámetro disminuye.

$$D_{n+a} = 0.8905257^a \cdot D_n$$

Como caso particular, si a = 6, entonces:

$$0.8905257^6 = 0.4987452 \text{ ? } 0.5 \text{ ? } D_{n+6} = 0.5 D_n$$

Por cada 6 números que aumenta el calibre, el diámetro se reduce a la mitad.

MANEJO DE TABLAS DE REACTANCIA INDUCTIVA

$$X_L = 0.00289 \log_{10} \frac{DMG}{RMG} \text{ ? / Km/ fase } + 0.00289 \log_{10} \frac{1}{RMG} + 0.00289 \log_{10} DMG$$

Por una parte, el primer término, representa la reactancia debida al flujo interno desde una distancia unitaria en cm, ft o m; dependiendo de las unidades del RMG. Por otra, el segundo término representa la reactancia debida al flujo externo desde la distancia unidad hasta la DMG.

$$X_i = 0.00465 \log \frac{DMG}{RMG} \text{ ? / milla / cond}$$

$$\text{si } x_a = 0.004657 \log \frac{1}{RMG} \text{ ? / milla / cond}$$

$$\text{y } x_b = 0.004657 \log DMG \text{ ? / milla / cond}$$

entonces

$$X_i = x_a + x_b$$



DIVISIÓN DE EDUCACIÓN
CONTINUA Y A DISTANCIA



ANEXOS

EXPOSITOR: ING. FERNANDO TOLEDO TOLEDO

SECRETARÍA DE LA DEFENSA NACIONAL

Annex 4A

Typical impedance data for short-circuit studies

(informative)

The following tables and figures appear in this annex:

Table 4A-1, Typical reactance values for induction and synchronous machines, in per-unit of machine kVA ratings

Table 4A-2, Representative conductor spacings for overhead lines

Table 4A-3, Constants of copper conductors for 1 ft symmetrical spacing

Table 4A-4, Constants of aluminum cable, steel reinforced (ACSR), for 1 ft symmetrical spacing

Table 4A-5, 60 Hz reactance spacing factor X_B , in ohms per conductor per 1000 ft

Table 4A-6, 60 Hz reactance spacing factor X_B , in ohms per conductor per 1000 ft

Table 4A-7, 60 Hz impedance data for three-phase copper cable circuits, in approximate ohms per 1000 ft at 75 °C (nonshielded varnished cambric/shielded neoprene insulated cables)

Table 4A-8, 60 Hz impedance data for three-phase aluminum cable circuits, in approximate ohms per 1000 ft at 90 °C (cross-linked polyethylene insulated cable)

Figure 4A-1, X/R ratio of transformers

Figure 4A-2, X/R range for small generators and synchronous motors (solid rotor and salient pole)

Figure 4A-3, X/R range for three-phase induction motors

The following tables appear in other chapters:

Table 10-15, BILs and percent impedance voltages at self-cooled (OA) rating for liquid-immersed transformers (Chapter 10)

Table 10-16, BILs and percent impedance voltage for dry-type transformers (Chapter 10)

Table 13-2, Voltage-drop values of three-phase, sandwiched busways with copper bus bars, in V/100 ft, line-to-line, at rated current with concentrated load (Chapter 13)

Table 13-3, Voltage-drop values of three-phase, sandwiched busways with aluminum bus bars, in V/100 ft, line-to-line, at rated current with concentrated load (Chapter 13)

Table 4A-1—Typical reactance values for induction and synchronous machines, in per unit of machine kVA ratings*

	X_d'	X_d''
Turbine generators†		
2 poles	0.09	0.15
4 poles	0.15	0.23
Salient-pole generators with damper windings†		
12 poles or less	0.16	0.33
14 poles or less	0.21	0.33
Synchronous motors		
6 poles	0.15	0.23
8–14 poles	0.20	0.30
16 poles or more	0.28	0.40
Synchronous condensers†	0.24	0.37
Synchronous converters†		
600 V direct current	0.20	—
250 V direct current	0.33	—
Individual large induction motors, usually above 600 V	0.17	—
Smaller motors, usually 600 V and below	See tables 4-1 and 4-2.	

NOTE—Approximate synchronous motor kVA bases can be found from motor horsepower ratings as follows:

0.8 power factor motor—kVA base = hp rating

1.0 power factor motor—kVA base = 0.8 · hp rating

*Use manufacturer's specified values if available.

† X_d' not normally used in short-circuit calculations.

Table 4A-2—Representative conductor spacings for overhead lines

Nominal system voltage (volts)	Equivalent delta spacing (inches)
120	12
240	12
480	18
600	18
2400	30
4160	30
6900	36
13 800	42
23 000	48
34 500	54
69 000	96
115 000	204

NOTE—When the cross section indicates conductors are arranged at points of a triangle with spacings *A*, *B*, and *C* between pairs of conductors, the following formula may be used:

$$\text{equivalent delta spacing} = \sqrt[3]{A \cdot B \cdot C}$$

When the conductors are located in one place and the outside conductors are equally spaced at distance *A* from the middle conductors, the equivalent is 1.26 times the distance *A*:

$$\begin{aligned} \text{equivalent delta spacing} &= \sqrt[3]{A \cdot A \cdot 2A} \\ &= 1.26A \end{aligned}$$

Table 4A-3—Constants of copper conductors for 1 ft symmetrical spacing*

Size of conductor		Resistance R at 50 °C, 60 Hz	Reactance X_A at 1 ft spacing, 60 Hz
(cmil)	(AWG No.)	(Ω /conductor/1000 ft)	(Ω /conductor/1000 ft)
1 000 000		0.0130	0.0758
900 000		0.142	0.0769
800 000		0.0159	0.0782
750 000		0.0168	0.0790
700 000		0.0179	0.0800
600 000		0.0206	0.0818
500 000		0.0246	0.0839
450 000		0.0273	0.0854
400 000		0.0307	0.0867
350 000		0.0348	0.0883
300 000		0.0407	0.0902
250 000		0.0487	0.0922
211 600	4/0	0.0574	0.0953
167 800	3/0	0.0724	0.0981
133 100	2/0	0.0911	0.101
105 500	1/0	0.115	0.103
83 690	1	0.145	0.106
66 370	2	0.181	0.108
52 630	3	0.227	0.111
41 740	4	0.288	0.113
33 100	5	0.362	0.116
26 250	6	0.453	0.121
20 800	7	0.570	0.123
16 510	8	0.720	0.126

NOTE—For a three-phase circuit the total impedance, line to neutral, is $Z = R + j(X_A + X_B)$.

*Use spacing factors of X_B of tables 4A-5 and 4A-6 for other spacings.

Table 4A-4—Constants of aluminum cable, steel reinforced (ACSR), for 1 ft symmetrical spacing*

Size of conductor		Resistance R at 50 °C, 60 Hz	Reactance X_A at 1 ft spacing, 60 Hz
(cmil)	(AWG No.)	(Ω /conductor/1000 ft)	(Ω /conductor/1000 ft)
1 590 000		0.0129	0.0679
1 431 000		0.0144	0.0692
1 272 000		0.0161	0.0704
1 192 500		0.0171	0.0712
1 113 000		0.0183	0.0719
954 000		0.0213	0.0738
795 000		0.0243	0.0744
715 500		0.0273	0.0756
636 000		0.0307	0.0768
556 500		0.0352	0.0786
477 000		0.0371	0.0802
397 500		0.0445	0.0824
336 400		0.0526	0.0843
266 800		0.0662	0.0945
	4/0	0.0835	0.1099
	3/0	0.1052	0.1175
	2/0	0.1330	0.1212
	1/0	0.1674	0.1242
	1	0.2120	0.1259
	2	0.2670	0.1215
	3	0.3370	0.1251
	4	0.4240	0.1240
	5	0.5340	0.1259
	6	0.6740	0.1273

NOTE—For a three-phase circuit the total impedance, line to neutral, is $Z = R + j(X_A + X_B)$.

*Use spacing factors of X_B from tables 4A-5 and 4A-6 for other spacings.

**Table 4A-6—60 Hz reactance spacing factor X_B ,
in ohms per conductor per 1000 ft**

Separation (quarter inches)				
(inches)	0	1/4	2/4	3/4
0	—	—	-0.072 9	-0.063 6
1	-0.0571	-0.051 9	-0.047 7	-0.044 3
2	-0.0412	-0.038 4	-0.035 9	-0.033 9
3	-0.0319	-0.030 1	-0.028 2	-0.026 7
4	-0.0252	-0.023 8	-0.022 5	-0.021 2
5	-0.0201	-0.017 95	-0.017 95	-0.016 84
6	-0.0159	-0.014 94	-0.013 99	-0.013 23
7	-0.0124	-0.011 52	-0.010 78	-0.010 02
8	-0.0093	-0.008 52	-0.007 94	-0.007 19
9	-0.0066	-0.006 05	-0.005 29	-0.004 74
10	-0.0042	—	—	—
11	-0.0020	—	—	—
12	—	—	—	—

Table 4A-7—60 Hz impedance data for three-phase copper cable circuits, in approximate ohms per 1000 ft at 75 °C
(a) Three single conductors

AWG or kcmil	In magnetic duct						In nonmagnetic duct					
	600 V and 5 kV nonshielded			5 kV shielded and 15 kV			600 V and 5 kV nonshielded			5 kV shielded and 15 kV		
	R	X	Z	R	X	Z	R	X	Z	R	X	Z
8	0.811	0.0754	0.814	0.811	0.0860	0.816	0.811	0.0603	0.813	0.811	0.0688	0.814
8 (solid)	0.786	0.0754	0.790	0.786	0.0860	0.791	0.786	0.0603	0.788	0.786	0.0688	0.789
6	0.510	0.0685	0.515	0.510	0.0796	0.516	0.510	0.0548	0.513	0.510	0.0636	0.514
6 (solid)	0.496	0.0685	0.501	0.496	0.0796	0.502	0.496	0.0548	0.499	0.496	0.0636	0.500
4	0.321	0.0632	0.327	0.321	0.0742	0.329	0.321	0.0506	0.325	0.321	0.0594	0.326
4 (solid)	0.312	0.0632	0.318	0.312	0.0742	0.321	0.312	0.0506	0.316	0.312	0.0594	0.318
2	0.202	0.0585	0.210	0.202	0.0685	0.214	0.202	0.0467	0.207	0.202	0.0547	0.209
1	0.160	0.0570	0.170	0.160	0.0675	0.174	0.160	0.0456	0.166	0.160	0.0540	0.169
1/0	0.128	0.0540	0.139	0.128	0.0635	0.143	0.127	0.0432	0.134	0.128	0.0507	0.138
2/0	0.102	0.0533	0.115	0.103	0.0630	0.121	0.101	0.0426	0.110	0.102	0.0504	0.114
3/0	0.0805	0.0519	0.0958	0.0814	0.0605	0.101	0.0766	0.0415	0.0871	0.0805	0.0484	0.0939
4/0	0.0640	0.0497	0.0810	0.0650	0.0583	0.0929	0.0633	0.0398	0.0748	0.0640	0.0466	0.0792
250	0.0552	0.0495	0.0742	0.0557	0.0570	0.0797	0.0541	0.0396	0.0670	0.0547	0.0456	0.0712
300	0.0464	0.0493	0.0677	0.0473	0.0564	0.0736	0.0451	0.0394	0.0599	0.0460	0.0451	0.0644
350	0.0378	0.0491	0.0617	0.0386	0.0562	0.0681	0.0368	0.0393	0.0536	0.0375	0.0450	0.0586
400	0.0356	0.0490	0.0606	0.0362	0.0548	0.0657	0.0342	0.0392	0.0520	0.0348	0.0438	0.0559
450	0.0322	0.0480	0.0578	0.0328	0.0538	0.0630	0.0304	0.0384	0.0490	0.0312	0.0430	0.0531
500	0.0294	0.0466	0.0551	0.0300	0.0526	0.0505	0.0276	0.0373	0.0464	0.0284	0.0421	0.0508
600	0.0257	0.0463	0.0530	0.0264	0.0516	0.0580	0.0237	0.0371	0.0440	0.0246	0.0412	0.0479
750	0.0216	0.0445	0.0495	0.0223	0.0497	0.0545	0.0194	0.0356	0.0405	0.0203	0.0396	0.0445

NOTE—Resistance based on tinned copper at 60 Hz; 600 V and 5 kV nonshielded cable based on varnished cambric insulation; 5 kV shielded and 15 kV cable based on neoprene insulation.

*Resistance values (R_L) at lower copper temperatures (T_L) are obtained by using the formula $R_L = \frac{R_{75}(234.5 + T_L)}{309.5}$.

Table 4A-7—60 Hz impedance data for three-phase copper cable circuits, in approximate ohms per 1000 ft at 75 °C*
(b) Three-conductor cable

AWG or kcmil	In magnetic duct and steel interlocked armor						In nonmagnetic duct and aluminum interlocked armor					
	600 V and 5 kV nonshielded			5 kV shielded and 15 kV			600 V and 5 kV nonshielded			5 kV shielded and 15 kV		
	R	X	Z	R	X	Z	R	X	Z	R	X	Z
8	0.811	0.0577	0.813	0.811	0.0658	0.814	0.811	0.0503	0.812	0.811	0.0574	0.813
8 (solid)	0.786	0.0577	0.788	0.786	0.0658	0.789	0.786	0.0503	0.787	0.786	0.0574	0.788
6	0.510	0.0525	0.513	0.510	0.0610	0.514	0.510	0.0457	0.512	0.510	0.0531	0.513
6 (solid)	0.496	0.0525	0.499	0.496	0.0610	0.500	0.496	0.0457	0.498	0.496	0.0531	0.499
4	0.321	0.0483	0.325	0.321	0.0568	0.326	0.321	0.0422	0.324	0.321	0.0495	0.325
4 (solid)	0.312	0.0483	0.316	0.312	0.0508	0.317	0.312	0.0422	0.315	0.312	0.0495	0.316
2	0.202	0.0448	0.207	0.202	0.0524	0.209	0.202	0.0390	0.206	0.202	0.0457	0.207
1	0.160	0.0436	0.166	0.160	0.0516	0.168	0.160	0.0380	0.164	0.160	0.0450	0.166
1/0	0.128	0.0414	0.135	0.128	0.0486	0.137	0.127	0.0360	0.132	0.128	0.0423	0.135
2/0	0.102	0.0407	0.110	0.103	0.0482	0.114	0.101	0.0355	0.107	0.102	0.0420	0.110
3/0	0.0805	0.0397	0.0898	0.0814	0.0463	0.0936	0.0766	0.0346	0.0841	0.0805	0.0403	0.090
4/0	0.0640	0.0381	0.0745	0.0650	0.0446	0.0788	0.0633	0.0332	0.0715	0.0640	0.0389	0.0749
250	0.0552	0.0379	0.0670	0.0557	0.0436	0.0707	0.0541	0.0330	0.0634	0.0547	0.0380	0.0666
300	0.0464	0.0377	0.0598	0.0473	0.0431	0.0640	0.0451	0.0329	0.0559	0.0460	0.0376	0.0596
350	0.0378	0.0373	0.0539	0.0386	0.0427	0.0576	0.0368	0.0328	0.0492	0.0375	0.0375	0.0530
400	0.0356	0.0371	0.0514	0.0362	0.0415	0.0551	0.0342	0.0327	0.0475	0.0348	0.0366	0.0505
450	0.0322	0.0361	0.0484	0.0328	0.0404	0.0520	0.0304	0.0320	0.0441	0.0312	0.0359	0.0476
500	0.0294	0.0349	0.0456	0.0300	0.0394	0.0495	0.0276	0.0311	0.0416	0.0284	0.0351	0.0453
600	0.0257	0.0343	0.0429	0.0264	0.0382	0.0464	0.0237	0.0309	0.0389	0.0246	0.0344	0.0422
750	0.0216	0.0326	0.0391	0.0223	0.0364	0.0427	0.0197	0.0297	0.0355	0.0203	0.0332	0.0389

NOTE—Resistance based on tinned copper at 60 Hz. 600 V and 5 kV nonshielded cable based on varnished cambric insulation; 5 kV shielded and 15 kV cable based on neoprene insulation

*Resistance values (R_L) at lower copper temperatures (T_L) are obtained by using the formula $R_L = \frac{R_{75} (234.5 + T_L)}{309.5}$.

Table 4A-8—60 Hz impedance data for three-phase aluminum cable circuits, in approximate ohms per 1000 ft at 90 °C*
(a) Three single conductors

AWG or kcmil	In magnetic duct						In nonmagnetic duct					
	600 V and 5 kV nonshielded			5 kV shielded and 15 kV			600 V and 5 kV nonshielded			5 kV shielded and 15 kV		
	R	X	Z	R	X	Z	R	X	Z	R	X	Z
6	0.847	0.053	0.849	—	—	—	0.847	0.042	0.848	—	—	—
4	0.532	0.050	0.534	0.532	0.068	0.536	0.532	0.040	0.534	0.532	0.054	0.535
2	0.335	0.046	0.338	0.335	0.063	0.341	0.335	0.037	0.337	0.335	0.050	0.339
1	0.265	0.048	0.269	0.265	0.059	0.271	0.265	0.035	0.267	0.265	0.047	0.269
1/0	0.210	0.043	0.214	0.210	0.056	0.217	0.210	0.034	0.213	0.210	0.045	0.215
2/0	0.167	0.041	0.172	0.167	0.055	0.176	0.167	0.033	0.170	0.167	0.044	0.173
3/0	0.133	0.040	0.139	0.132	0.053	0.142	0.133	0.037	0.137	0.132	0.042	0.139
4/0	0.106	0.039	0.113	0.105	0.051	0.117	0.105	0.031	0.109	0.105	0.041	0.113
250	0.0896	0.0384	0.0975	0.0892	0.0495	0.102	0.0894	0.0307	0.0945	0.0891	0.0396	0.0975
300	0.0750	0.0375	0.0839	0.0746	0.0479	0.0887	0.0746	0.0300	0.0804	0.0744	0.0383	0.0837
350	0.0644	0.0369	0.0742	0.0640	0.0468	0.0793	0.0640	0.0245	0.0705	0.0638	0.0374	0.0740
400	0.0568	0.0364	0.0675	0.0563	0.0459	0.0726	0.0563	0.0291	0.0634	0.0560	0.0367	0.0700
500	0.0459	0.0355	0.0580	0.0453	0.0444	0.0634	0.0453	0.0284	0.0535	0.0450	0.0355	0.0573
600	0.0388	0.0359	0.0529	0.0381	0.0431	0.0575	0.0381	0.0287	0.0477	0.0377	0.0345	0.0511
700	0.0338	0.0350	0.0487	0.0332	0.0423	0.0538	0.0330	0.0280	0.0433	0.0326	0.0338	0.0470
750	0.0318	0.0341	0.0466	0.0310	0.0419	0.0521	0.0309	0.0273	0.0412	0.0304	0.0335	0.0452
1000	0.0252	0.0341	0.0424	0.0243	0.0414	0.0480	0.0239	0.0273	0.0363	0.0234	0.0331	0.0405

NOTE—Cross-linked polyethylene insulated cable.

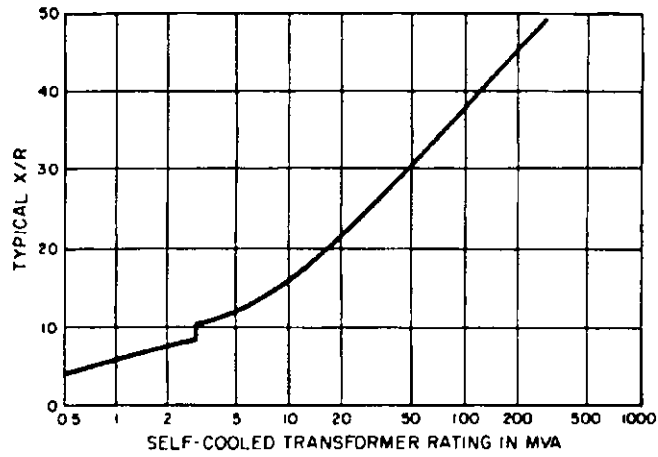
*Resistance values (R_L) at lower aluminum temperatures (T_L) are obtained by using the formula $R_L = \frac{R_{90} (228.1 + T_L)}{318.1}$.

Table 4A-8—60 Hz impedance data for three-phase aluminum cable circuits, in approximate ohms per 1000 ft at 90 °C*
(b) Three-conductor cable

AWG or kcmil	In magnetic duct						In nonmagnetic duct					
	600 V and 5 kV nonshielded			5 kV shielded and 15 kV			600 V and 5 kV nonshielded			5 kV shielded and 15 kV		
	R	X	Z	R	X	Z	R	X	Z	R	X	Z
6	0.847	0.053	0.849	—	—	—	0.847	0.042	0.848	—	—	—
4	0.532	0.050	0.534	—	—	—	0.532	0.040	0.534	—	—	—
2	0.335	0.046	0.338	0.335	0.056	0.340	0.335	0.037	0.337	0.335	0.045	0.338
1	0.265	0.048	0.269	0.265	0.053	0.270	0.265	0.035	0.267	0.265	0.042	0.268
1/0	0.210	0.043	0.214	0.210	0.050	0.216	0.210	0.034	0.213	0.210	0.040	0.214
2/0	0.167	0.041	0.172	0.167	0.049	0.174	0.167	0.033	0.170	0.167	0.039	0.171
3/0	0.133	0.040	0.139	0.133	0.048	0.141	0.133	0.037	0.137	0.132	0.038	0.138
4/0	0.106	0.039	0.113	0.105	0.045	0.114	0.105	0.031	0.109	0.105	0.036	0.111
250	0.0896	0.0384	0.0975	0.0895	0.0436	0.100	0.0894	0.0307	0.0945	0.0893	0.0349	0.0959
300	0.0750	0.0375	0.0839	0.0748	0.0424	0.0860	0.0746	0.0300	0.0804	0.0745	0.0340	0.0819
350	0.0644	0.0369	0.0742	0.0643	0.0418	0.0767	0.0640	0.0245	0.0705	0.0640	0.0334	0.0722
400	0.0568	0.0364	0.0675	0.0564	0.0411	0.0700	0.0563	0.0291	0.0634	0.0561	0.0329	0.0650
500	0.0459	0.0355	0.0580	0.0457	0.0399	0.0607	0.0453	0.0284	0.0535	0.0452	0.0319	0.0553
600	0.0388	0.0359	0.0529	0.0386	0.0390	0.0549	0.0381	0.0287	0.0477	0.0380	0.0312	0.0492
700	0.0338	0.0350	0.0487	0.0335	0.0381	0.0507	0.0330	0.0280	0.0433	0.0328	0.0305	0.0448
750	0.0318	0.0341	0.0466	0.0315	0.0379	0.0493	0.0309	0.0273	0.0412	0.0307	0.0303	0.0431
1000	0.0252	0.0341	0.0424	0.0248	0.0368	0.0444	0.0239	0.0273	0.0363	0.0237	0.0294	0.0378

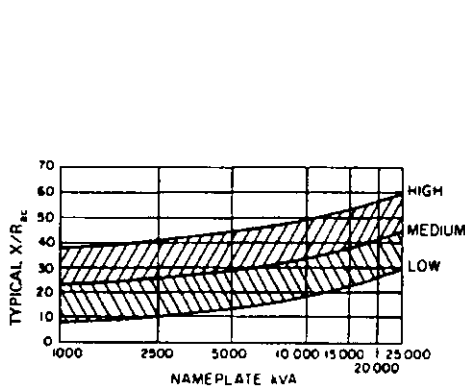
NOTE—Cross-linked polyethylene insulated cable.

*Resistance values (R_L) at lower aluminum temperatures (T_L) are obtained by the formula $R_L = \frac{R_{90} (228.1 + T_L)}{318.1}$.



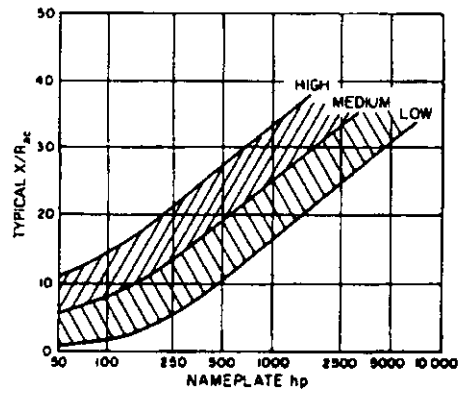
Source: Based on IEEE Std C37.010-1979.

Figure 4A-1— X/R ratio of transformers



Source: Reprinted from IEEE Std C37.010-1979.

Figure 4A-2— X/R range for small generators and synchronous motors (solid rotor and salient pole)



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Figure 4A-3— X/R range for three-phase induction motors

CHAPTER 3

CHARACTERISTICS OF AERIAL LINES

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IN the design, operation, and expansion of electrical power systems it is necessary to know electrical and physical characteristics of conductors used in the construction of aerial distribution and transmission lines.

This chapter presents a description of the common types of conductors along with calculations of their important electrical and physical characteristics. General formulas are presented with their derivation to show the basis of the tabulated values and as a guide in calculating data for other conductors of similar shapes, dimensions, composition and operating conditions.

All included are the more commonly used symmetrical, complete sequence input line equations that are applicable to the solution of power system problems involving voltage regulation, load flow, stability, system currents, and voltage under fault conditions, or other system problems where the electrical characteristics of aerial lines are involved.

Additional formulas are given to permit calculation of approximate current-carrying capacity of conductors taking into account such factors as convection and radiation losses as influenced by ambient temperature, wind velocity, and permissible temperature rise.

I. TYPES OF CONDUCTORS

In the electric-power field the following types of conductors are generally used on high-voltage power transmission lines: stranded copper conductors, hollow copper conductors, and ACSR (aluminum cable, steel reinforced).

Other types of conductors such as Copperweld and Copperweld copper conductors are also used for transmission and distribution lines. Use is made of Copperweld bronze, copper bronze, and steel for current-carrying conductors on rural lines, as overhead ground wires for transmission lines, as buried counterpoises at the base of transmission towers, and also for long river crossings.

A stranded conductor, typical of both copper and steel conductors in the larger sizes, is shown in Fig. 1. A stranded conductor is easier to handle and is more flexible than a solid conductor, particularly in the larger sizes.

A typical ACSR conductor is illustrated in Fig. 2. In this type of conductor, aluminum strands are wound about a core of stranded steel. Varying relationships between tensile strength and current-carrying capacity as well as overall size of conductor can be obtained by varying the proportions of steel and aluminum. By the use of a filler, such as paper, between the outer aluminum strands and the inner steel strands, a conductor of large diameter can be obtained for use in high voltage lines. This type of con-

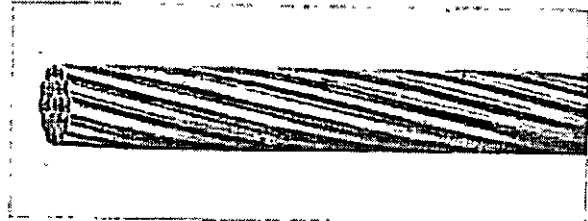


Fig. 1—A typical stranded conductor, (bare copper).

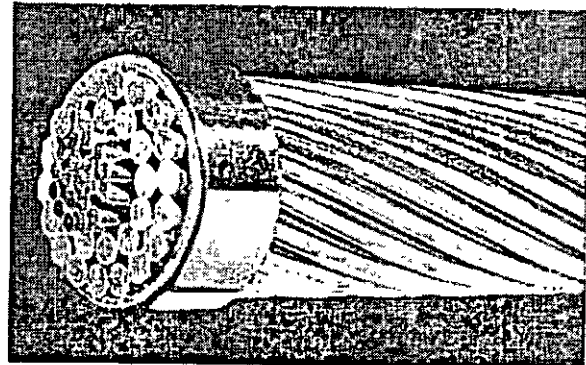


Fig. 2—A typical ACSR conductor.

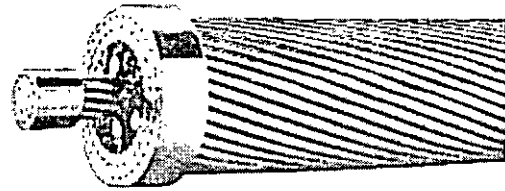


Fig. 3—A typical "expanded" ACSR conductor.



Fig. 4—A typical Anaconda Hollow Copper Conductor.

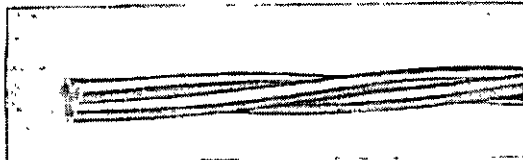
ductor is known as "expanded" ACSR and is shown in Fig. 3.

In Fig. 4 is shown a representative Anaconda Hollow Copper Conductor. It consists of a twisted copper "T"



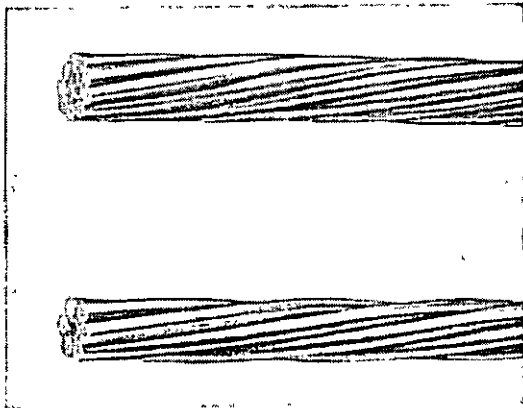
Courtesy of General Cable Corporation

Fig. 5—A typical General Cable Type III.



Courtesy of Copperweld Steel Company

Fig. 6—A typical Copperweld conductor.



Courtesy of Copperweld Steel Company

Fig. 7—Typical Copperweld-Copper conductors

- (a) Upper photograph—Type V
- (b) Lower photograph—Type R

beam as a core about which strands of copper wire are wound. The "I" beam is twisted in a direction opposite to that of the inner layer of strands.

Another form of hollow copper conductor is shown in Fig. 5. Known as the General Cable Type III hollow copper conductor, it is made up of segmental sections of copper mortised into each other to form a self-supporting hollow cylinder. Hollow copper conductors result in conductors of large diameter for a given cross section of copper. Corona losses are therefore smaller. This construction also produces a reduction in skin effect as well as inductance as compared with stranded conductors. A discussion of large diameter conductors and their characteristics is given in reference 1.

Copperweld conductors consist of different numbers of copper coated steel strands, a typical conductor being illustrated in Fig. 6. Strength is provided by the core of steel and protection by the outer coating of copper.

When high current-carrying capacities are desired as well as high tensile strength, copper strands are used with Copperweld strands to form Copperweld-Copper conduct-

ors as shown in Fig. 7. Different relationships between current-carrying capacity, outside diameter, and tensile strength can be obtained by varying the number and size of the Copperweld and copper strands.

II. ELECTRICAL CHARACTERISTICS OF AERIAL CONDUCTORS

The following discussion is primarily concerned with the development of electrical characteristics and constants of aerial conductors, particularly those required for analysis of power-system problems. The constants developed are particularly useful in the application of the principles of symmetrical components to the solution of power-system problems involving positive, negative, and zero-sequence impedances of transmission and distribution lines. The basic quantities needed are the positive, negative, and zero-sequence resistances, inductive reactances and shunt capacitive reactances of the various types of conductors and some general equations showing how these quantities are used.

I. Positive- and Negative-Sequence Resistance

The resistance of an aerial conductor is affected by the three factors: temperature, frequency, current density. Practical formulas and methods will now be given to take into account these factors.

Temperature Effect on Resistance—The resistance of copper and aluminum conductors varies almost directly with temperature. While this variation is not strictly linear for an extremely wide range of temperatures, for practical purposes it can be considered linear over the range of temperatures normally encountered.

When the d-c resistance of a conductor at a given temperature is known and it is desired to find the d-c resistance at some other temperature, the following general formula may be used.

$$\frac{R_{t_2}}{R_{t_1}} = \frac{M + t_2}{M + t_1} \tag{1}$$

where

- R_{t_2} = d-c resistance at any temperature t_2 , degree C
- R_{t_1} = d-c resistance at any other temperature t_1 , degree C.
- M = a constant for any one type of conductor material.
- = inferred absolute zero temperature.
- = 231.5 for annealed 100 percent conductivity copper.
- = 241.5 for hard drawn 97.3 percent conductivity copper.
- = 228.1 for aluminum.

The above formula is useful for evaluating changes in d-c resistance only, and cannot be used to give a-c resistance variations unless skin effect can be neglected. For small conductor sizes the frequency has a negligible effect on resistance in the d-c to 60-cycle range. This is generally true for conductor sizes up to 2.0.

The variations of resistance with temperature are usually unimportant because the actual ambient temperature is indefinite as well as variable along a transmission line. An illustration of percentage change in resistance is when temperature varies from winter to summer over a range of 60 degree C to 100 degrees C (132 degrees F to 101 degrees F) in which case copper resistance increases 17 percent.

TABLE 3-A—CHARACTERISTICS OF ANACONDA HOLLOW COPPER CONDUCTORS



(Anaconda Wire & Cable Company)

Design Number	Size of Conductor Mils or A.W.G.	Wire		Outside Diameter Inches	Breaking Strength Pounds	Weight Pounds per Mile	Geometric Mean Radius at 60 Cycles Feet	Approx. Current-Carrying Capacity Amps*	Resistance R_a Ohms per Conductor per Mile				Inductive Reactance X_L Ohms per Conductor per Mile at 1 Ft. Spacing			Shunt Capacitive Reactance X_C Megohms per Conductor per Mile at 1 Ft. Spacing					
		Number	Diameter Inches						25°C. (77°F.)				50°C. (122°F.)			25 cycles	50 cycles	60 cycles	25 cycles	50 cycles	60 cycles
									d-c	25 cycles	50 cycles	60 cycles	d-c	25 cycles	50 cycles						
									25 cycles	50 cycles	60 cycles	25 cycles	50 cycles	60 cycles							
909	600 609	25	0.1610	1.550	30 000	15 063	0.0012	1395	0.0974	0.0076	0.0734	0.0739	0.1412	0.282	0.339	0.1007	0.0055	0.0704			
901	119 400	12	0.0236	0.470	5 300	2 015	0.0165	210	0.491	0.491	0.517	0.517	0.203	0.407	0.407	0.408	0.299	0.1167	0.1167		

*For conductor at 75°C., air at 25°C., wind 1.4 miles per hour (3 1/4 m.p.h.), frequency=60 cycles, average larnished surface.

TABLE 3-B—CHARACTERISTICS OF GENERAL CABLE TYPE III HOLLOW COPPER CONDUCTORS

(General Cable Corporation)

Conductor Size Circular Mils or A.W.G.	Out-side Diameter Inches	Wall Thickness Inches	Weight Pounds per Mile	Breaking Strength Pounds	Geometric Mean Radius Feet	Approx. Current-Carrying Capacity Amps*	Resistance R_a Ohms per Conductor per Mile						Inductive Reactance X_L Ohms per Conductor per Mile at 1 Foot Spacing			Shunt Capacitive Reactance X_C Megohms per Conductor per Mile at 1 Foot Spacing					
							25°C. (77°F.)						50°C. (122°F.)			25 cycles	50 cycles	60 cycles	25 cycles	50 cycles	60 cycles
							d-c	25 cycles	50 cycles	60 cycles	d-c	25 cycles	50 cycles								
							25 cycles	50 cycles	60 cycles	25 cycles	50 cycles	60 cycles									
1 000 000	2.103	0.167	18 160	45 190	0.0832	1620	0.0378	0.0378	0.0377	0.0377	0.0630	0.0630	0.0631	0.0631	0.1257	0.251	0.302	0.1731	0.0067	0.0782	
2/0	0.500	0.0891	2 146	5 719	0.0195	382	0.432	0.432	0.432	0.432	0.472	0.472	0.472	0.201	0.403	0.403	0.483	0.276	0.1378	0.1149	

Notes: *Thickness at edge of interlocked segments. †Thickness uniform throughout.
(1) Conductors of smaller diameter for given cross-sectional area also available; in the larger sizes, some additional diameter expansion is possible.
(2) For conductor at 75°C., air at 25°C., wind 1.4 miles per hour (3 1/4 m.p.h.), frequency=60 cycles.

TABLE 4-A—CHARACTERISTICS OF COPPERWELD-COPPER CONDUCTORS (Copperweld Steel Company)

Table with columns for Nominal Designation, Size of Conductor, Copper Equivalent, Rated Breaking Load, Approx. Current-Carrying Capacity, Resistance (Ra), Reactance (Xa), Inductive Reactance (Xl), and Capacitive Reactance (Xc). Rows include various conductor sizes like 350 EK, 250 EK, 150 EK, 100 EK, 75 EK, 50 EK, 35 EK, 25 EK, 15 EK, 10 EK, 7.5 EK, 5 EK, 3.5 EK, 2.5 EK, 1.5 EK, 1 EK, 0.75 EK, 0.5 EK, 0.35 EK, 0.25 EK, 0.15 EK, 0.1 EK, 0.075 EK, 0.05 EK, 0.035 EK, 0.025 EK, 0.015 EK, 0.01 EK, 0.0075 EK, 0.005 EK, 0.0035 EK, 0.0025 EK, 0.0015 EK, 0.001 EK.

*Based on a conductor temperature of 75°C. and an ambient of 25°C., and 1 ft. min. per hour (3 ft./sec.), frequency = 60 cycles, average finished surface.
**Resistance at 50°C. total temperature, based on an ambient of 25°C. plus 25°C. rise due to heating effect of current. The approximate magnitude of current necessary to produce the 25°C. rise is 75% of the approximate current-carrying capacity at 60 cycles.

finding the appropriate table for a particular conductor. For these figures open circles, solid circles, and cross-hatched circles represent copper, steel, and aluminum conductors respectively. The double cross hatched area in the insert for Table 2-B, Characteristics of "EXPANDED"

Aluminum Cable Steel Reinforced, represents stranded paper. The authors wish to acknowledge the cooperation of the conductor manufacturers in supplying the information for compiling these tables.

CHAPTER 4

ELECTRICAL CHARACTERISTICS OF CABLES

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Revised by:

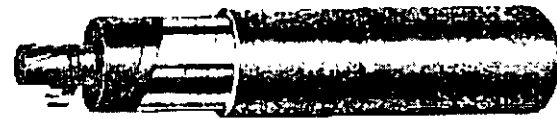
J. S. Williams

CABLES are classified according to their insulation as paper, varnished-paper, rubber, or asbestos, each of these materials having unique characteristics which render it suitable for particular applications. Because cables for power transmission and distribution are composed of so many different types of insulation, conductors, and sheathing materials, the discussion here must be limited to those cable designs most commonly used. Reasonable estimates of electrical characteristics for cables not listed can be obtained in most cases by reading from the table for a cable having similar physical dimensions.

Paper can be wound onto a conductor in successive layers to achieve a required dielectric strength, and this is the insulation generally used for cables operating at 10,000 volts and higher. Paper insulation is impregnated in different ways, and accordingly cables so insulated can be subdivided into solid, oil-filled, or gas-filled types.

Solid paper-insulated cables are built up of layers of paper tape wound onto the conductor and impregnated with a viscous oil, over which is applied a tight-fitting, extruded lead sheath. Multi-conductor solid cables are also available, but the material shown here covers only single- and three-conductor types. Three-conductor cables are of either belted or shielded construction. The belted assembly consists of the three separately insulated conductors cabled together and wrapped with another layer of impregnated paper, or belt, before the sheath is applied. In the shielded construction each conductor is individually insulated and covered with a thin metallic non-magnetic shielding tape; the three conductors are then cabled together, wrapped with a metallic binder tape, and sheathed with lead. The purpose of the metallic shielding tape around each insulated conductor is to control the electrostatic stress, reduce corona formation, and decrease the thermal resistance. To minimize circulating current under normal operating conditions and thus limit the power loss, shielding tape only three mils in thickness is used. Solid single-conductor cables are standard for all voltages from 1 to 60 kv; solid three-conductor cables are standard from 1 to 10 kv. Sample sections of paper-insulated single-conductor, three-conductor belted, and three-conductor shielded cables are shown in Fig. 1(a), (b), and (c) respectively.

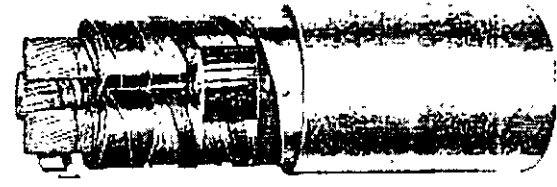
Oil-filled paper-insulated cables are available in single- or three-conductor designs. Single-conductor oil-filled cable consists of a concentric stranded conductor built around an open helical spring core, which serves as a channel for the flow of low-viscosity oil. This cable is insulated and sheathed in the same manner as solid cables, as a comparison of Figs. 1(c) and 1(d) indicates. Three-conductor oil-filled cables are all of the shielded design, and have three



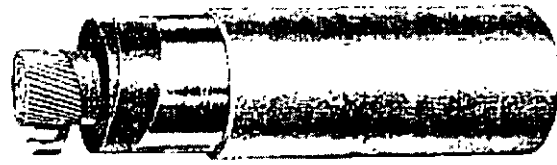
(a) Single-conductor solid, compact round conductor



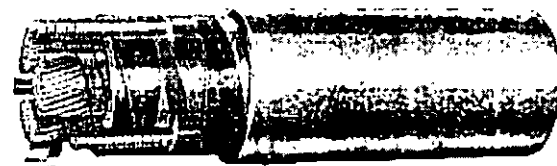
(b) Three-conductor belted, compact-sector conductors



(c) Three-conductor shielded, compact-sector conductors



(d) Single-conductor oil-filled, hollow-stranded conductor



(e) Three-conductor oil-filled, compact-sector conductors

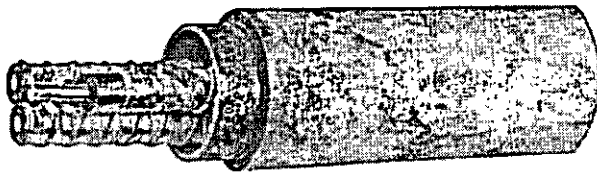
Fig. 1 Paper-insulated cables.

(Courtesy of General Cable Corporation)

oil channels composed of helical springs that extend through the cable in spaces normally occupied by filler material. This construction is shown in Fig. 1(d). Oil-filled cables are relatively new and their application has become widespread in a comparatively short time. The oil used is only slightly more viscous than transformer oil, and

remains fluid at all operating temperatures. The oil in the cable and its connected reservoirs is maintained under moderate pressure so that during load cycles oil may flow between the cable and the reservoirs to prevent the development of voids or excessive pressure in the cable. The prevention of void formation in paper insulation permits the use of greatly reduced insulation thickness for a given operating voltage. Another advantage of oil-filled cables is that oil will seep out through any crack or opening which develops in the sheath, thereby preventing the entrance of water at the defective point. This action prevents the occurrence of a fault caused by moisture in the insulation, and since operating records show that this cause accounts for a significant percentage of all high-voltage cable faults, it is indeed a real advantage. Single-conductor oil-filled cables are used for voltages ranging from 69 to 230 kv; the usual range for three-conductor oil-filled cables is from 23 to 69 kv.

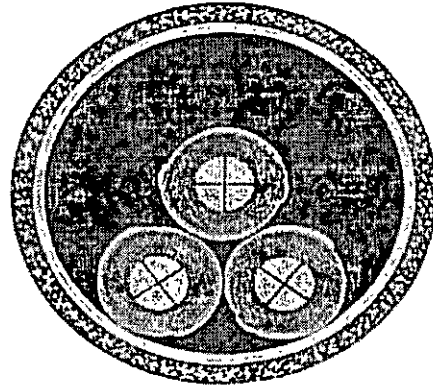
Gas-filled cables of the low-pressure type have recently become standard up to 46 kv. The single-conductor type employs construction generally similar to that of solid cables, except that longitudinal flutes or other channels are provided at the inner surface of the sheath to conduct nitrogen along the cable. The three-conductor design employs channels in the filler spaces among the conductors, much like those provided in oil-filled three-conductor cables. The gas is normally maintained between 10 and 15 pounds per square inch gauge pressure, and serves to fill all cable voids and exclude moisture at faulty points in the sheath or joints.



Courtesy of the Okonite-Gallender Cable Company

Fig. 2—High-pressure pipe-type oil-filled cable.

High-pressure cables, of either the oil- or gas-filled variety, are being used widely for the higher range of voltages. The physical and electrical characteristics are fairly well known, but their specifications are not yet standardized. The usual application calls for pressure of about 200 pounds per square inch, contained by a steel pipe into which three single-conductor cables are pulled. The immediate presence of the iron pipe makes difficult the calculations of circuit impedance, particularly the zero-sequence quantities. Most high-pressure cables are designed so that the oil or gas filler comes into direct contact with the conductor insulation; in oil-filled pipe-type cables a temporary lead sheath can be stripped from the cable as it is pulled into the steel pipe; in gas-filled pipe-type cables the lead sheath surrounding each conductor remains in place, with nitrogen introduced both inside and outside the sheath so that no differential pressure develops across the sheath. Examples of oil- and gas-filled pipe-type cables are shown in Figs. 2 and 3.



Courtesy of General Cable Corporation

Fig. 3—Cross-section of high-pressure pipe-type gas-filled cable. Oil-filled pipe-type cable may have a similar cross-section.

Compression cable is another high-pressure pipe-type cable in which oil or nitrogen gas at high pressure is introduced within a steel pipe containing lead-sheathed solid-type single-conductor cables; no high-pressure oil or gas is introduced directly inside the lead sheaths, but voids within the solid-type insulation are prevented by pressure exerted externally on the sheaths. This construction is sketched in Fig. 4.

During recent years there has been a trend toward the modification of cable conductors to reduce cost and improve operating characteristics, particularly in multi-conductor cables. Referring to Fig. 5, the first departure from concentric round conductors was the adoption of sector-shaped conductors in three-conductor cables. More recently a crushed stranding that results in a compacted sector has been developed and has found widespread use for conductor sizes of 1/0 A.W.G. and larger. Its use in smaller conductors is not practical. The principal advantages of such a conductor are: reduced overall diameter for a given copper cross-section; elimination of space between the conductor and the insulation, which results in higher

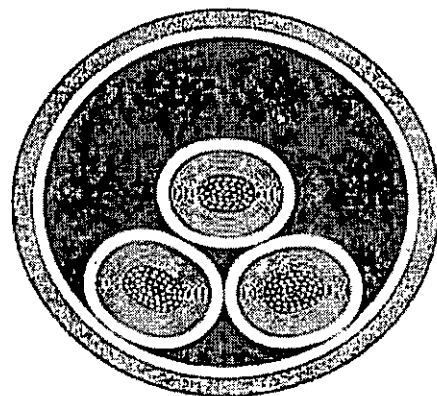
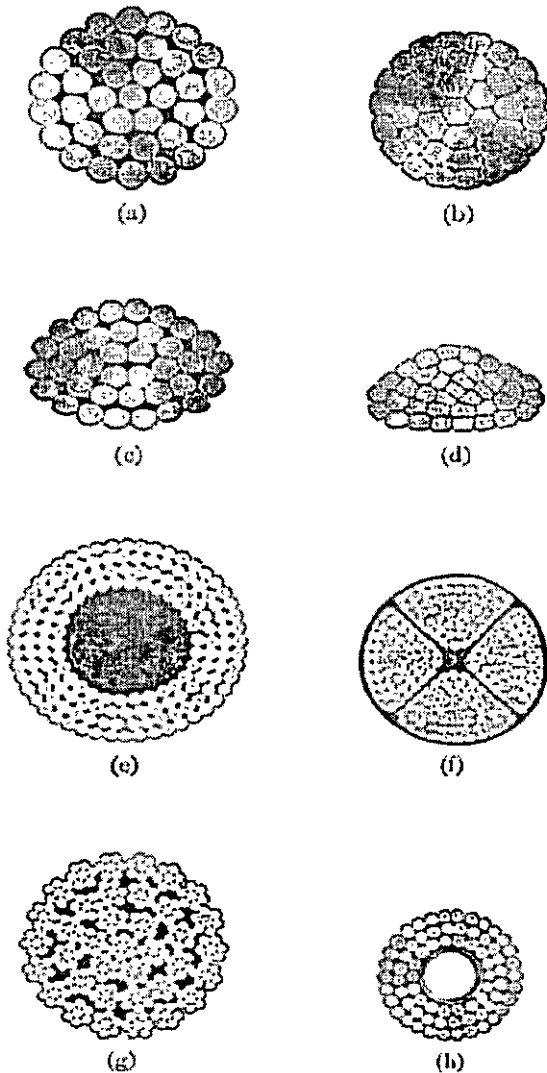


Fig. 4—Cross-sectional sketch of compression cable.



Photographs in this figure furnished by the Oliver-Ro-Catender Cable Company

Fig. 5—Cable conductors.

- (a) Standard concentric stranded.
- (b) Compact round.
- (c) Non-compact sector.
- (d) Compact sector.
- (e) Annular stranded (rope core).
- (f) Segmental.
- (g) Rope stranded.
- (h) Hollow core.

electrical breakdown; low a-c resistance due to minimizing of proximity effect; retention of the close stranding during bending; and for solid cables, elimination of many longitudinal channels along which impregnating compound can migrate. While most single-conductor cables are of the

concentric-strand type, they may also be compact-round, annular-stranded, segmental, or hollow-core.

I. ELECTRICAL CHARACTERISTICS

The electrical characteristics of cables have been discussed comprehensively in a series of articles¹ upon which much of the material presented here has been based. This chapter is primarily concerned with the determination of the electrical constants most commonly needed for power-system calculations, particular emphasis being placed on quantities necessary for the application of symmetrical components.² A general rule is that regardless of the complexity of mutual inductive relations between component parts of individual phases, the method of symmetrical components can be applied rigorously whenever there is symmetry among phases. All the three-conductor cables inherently satisfy this condition by the nature of their construction; single-conductor cables may or may not, although usually the error is small in calculating short-circuit currents. Unsymmetrical spacing and change in permeability resulting from different phase currents when certain methods of eliminating sheath currents are used, may produce dissymmetry.

Those physical characteristics that are of general interest in electrical application problems have been included along with electrical characteristics in the tables of this section.

All linear dimensions of radius, diameter, separation, or distance to equivalent earth return are expressed in inches in the equations in this chapter. This is unlike overhead transmission line theory where dimensions are in feet; the use of inches when dealing with cable construction seems appropriate. Many equations contain a factor for frequency, f , which is the circuit operating frequency in cycles per second.

1. Geometry of Cables

The space relationship among sheaths and conductors in a cable circuit is a major factor in determining reactance, capacitance, charging current, insulation resistance, dielectric loss, and thermal resistance. The symbols used in this chapter for various cable dimensions, both for single-conductor and three-conductor types, are given in Figs. 6 and 7. Several factors have come into universal use for defining the cross-section geometry of a cable circuit, and some of these are covered in the following paragraphs.^{1,2}

Geometric Mean Radius (GMR)—This factor is a property usually applied to the conductor alone, and depends on the material and stranding used in its construction. One component of conductor reactance³ is normally calculated by evaluating the integrated flux-linkages both inside and outside the conductor within an overall twelve-inch radius. Considering a solid conductor, some of the flux lines lie within the conductor and contribute to total flux-linkages even though they link only a portion of the total conductor current; if a tubular conductor having an infinitely thin wall were substituted for the solid conductor, its flux would necessarily all be external to the tube. A theoretical tubular conductor, in order to be inductively equivalent to a solid conductor, must have a smaller radius so

TABLE 1—CHARACTERISTICS OF COPPER CONDUCTORS, HARD DRAWN, 97.3 PERCENT CONDUCTIVITY



Table with columns: Size of Conductor (Circular Mils, A.W.G. or B.C.), Diameter of Individual Strands, Outside Diameter, Breaking Strength, Weight per Mile, Approx Current Carrying Capacity, Geometric Mean Radius, Resistance (Ohms per Conductor per Mile) at 25°C and 50°C for different cycles, Inductive Reactance, and Shunt Capacitive Reactance.

* For conductor at 75°C., air at 25°C., wind 1.4 miles per hour (2 ft/sec), frequency = 60 cycles.

carrying capacity based on 50°C rise above an ambient of 25°C, (75°C total conductor temperature), tarnished surface (E = 0.5), and an air velocity of 2 feet per second. These conditions were used after discussion and agreement with the conductor manufacturers. These thermal limitations are based on continuous loading of the conductors.

The technical literature shows little variation from these conditions as line design limits. The ambient air temperature is generally assumed to be 25°C to 40°C whereas the temperature rise is assumed to be 10°C to 60°C. This gives a conductor total temperature range of 35°C to 100°C. For design purposes copper or ACSR conductor total temperature is usually assumed to be 75°C as use of this value has given good conductor performance from an annealing standpoint, the limit being about 100°C where annealing of copper and aluminum begins.

Using Schurig and Frick's formulas, Fig. 25 and Fig. 26 have been calculated to show how current-carrying capacity of copper and aluminum conductors varies with ambient temperature assuming a conductor temperature of 75°C and wind velocity of 2 feet per second. These values are conservative and can be used as a guide in normal line design. For those lines where a higher conductor tem-

perature may be obtained that approaches 100°C, the conductor manufacturer should be consulted for test data or other more accurate information as to conductor temperature limitations. Such data on copper conductors has been presented rather thoroughly in the technical literature.7

III TABLES OF CONDUCTOR CHARACTERISTICS

The following tables contain data on copper, ACSR, hollow copper, Copperweld-copper, and Copperweld conductors, which along with the previously derived equations, permit the determination of positive-, negative-, and zero-sequence impedances of conductors for use in the solution of power-system problems. Also tabulated are such conductor characteristics as size, weight, and current-carrying capacity as limited by heating.

The conductor data (r_a, x_a, x_a') along with inductive and shunt-capacitive reactance spacing factors (x_d, x_d') and zero-sequence resistance, inductive and shunt-capacitive reactance factors (r_e, x_e, x_e') permit easy substitution in the previously derived equations for determining the symmetrical component sequence impedances of aerial circuits.

The cross-sectional inserts in the tables are for ease in